

Imp/Or Ideas in Non-Ideal MHD

→ Freezing-in law:

$$\frac{d \underline{B}}{dt} = \underline{B} \cdot \nabla \underline{V} + \eta \nabla^2 \underline{B}$$

↑
breaking \rightarrow small scale \rightarrow singularity

turbulence

→



→ current sheet
singular layers

→ sites of reconnection \rightarrow boundary layer problem

→ topology changes

→ so

- Sweet-Parker Reconnection theory

- Re-visiting magnetic helicity - Taylor Theory

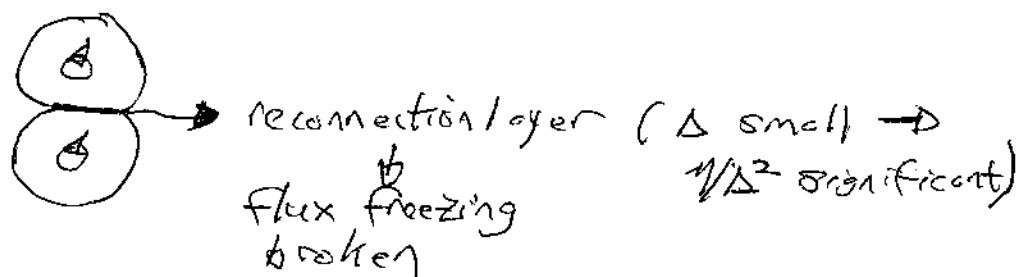
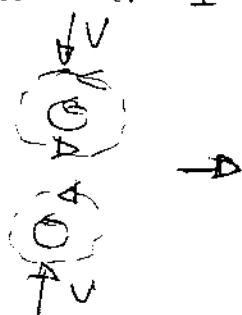
- anomalous resistivity (again)

- flux expulsion

→ Breakdown of Flux Freezing - Magnetic Reconnection $\cancel{?}$

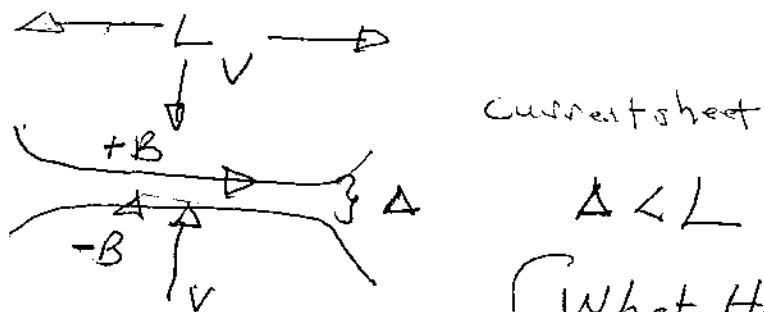
Simple Example : Sweet - Parker Problem
(re-visit later)

→ consider two cylinders of plasma, carrying current \perp plane, brought together



→ consider Layer

2 plasma slabs
brought together
at v



$$\nabla \cdot \underline{v} = 0 \quad \frac{d \underline{B}}{dt} = \underline{B} \cdot \nabla \underline{v} + \nabla \cdot \underline{\nabla B}$$

{ What Happens ?
Stationary
Solution
Possible ?

$$S_{ij}^{(0)} = \begin{pmatrix} 0 & 0 \\ 0 & -V_{0yy} \end{pmatrix}$$

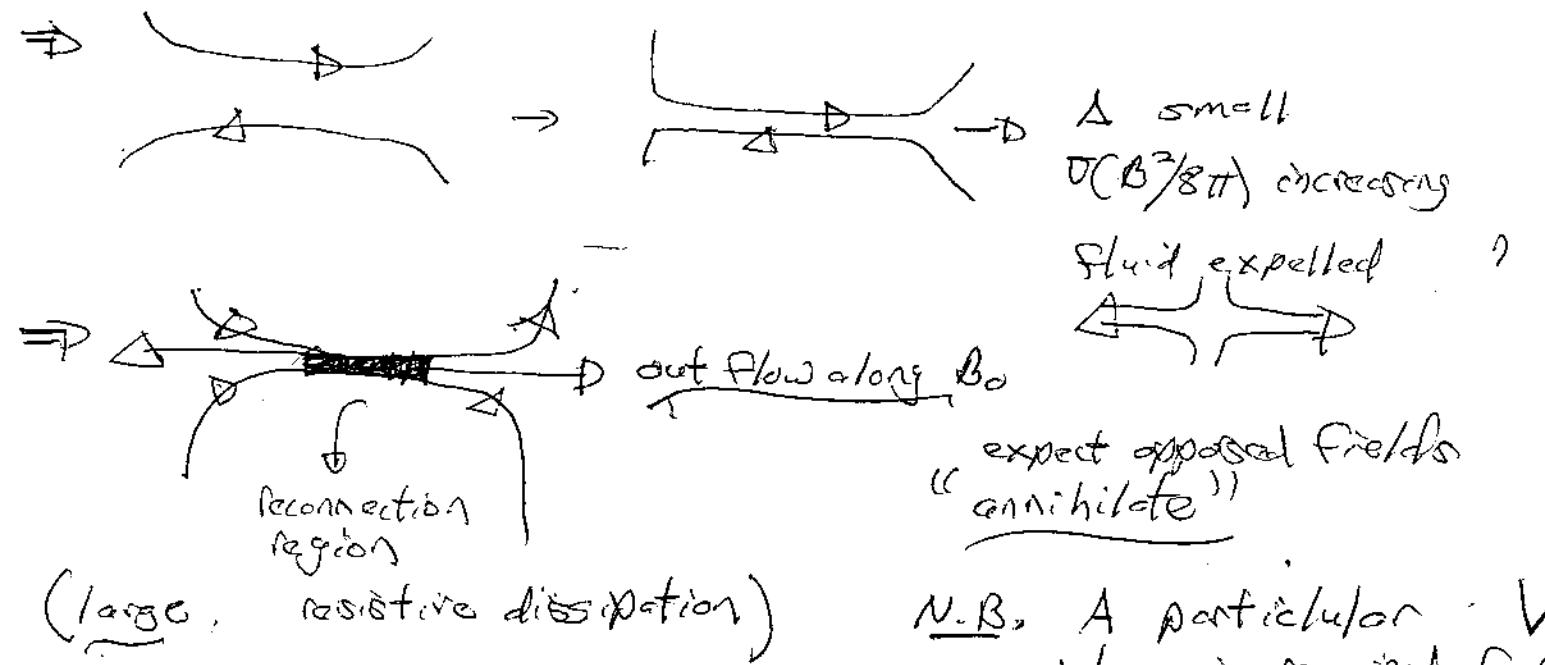
Rate-of-strain tensor

singularity

tip-off. of small scale generation in \underline{B}
⇒ resistive diffusion, breaking of freezing in ...

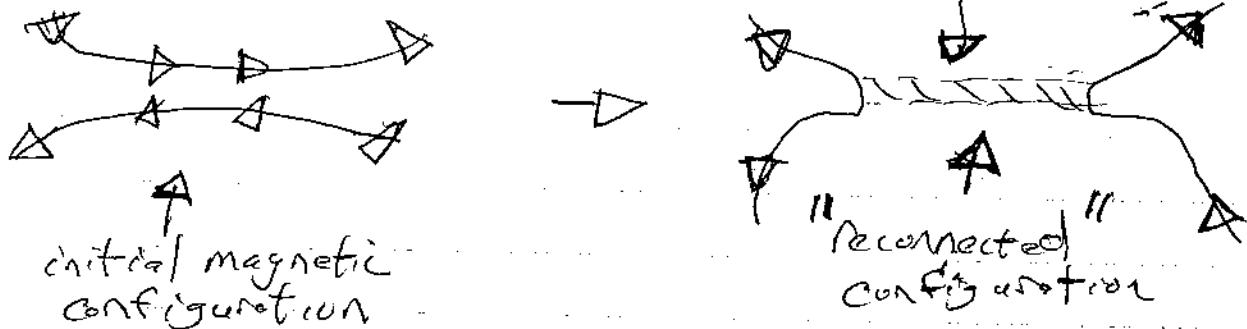
i.e. for stationary solution,

$$-\frac{\underline{B} \cdot \nabla V}{\eta} = \nabla^2 \underline{B}, \quad \nabla \cdot \underline{V} = 0$$

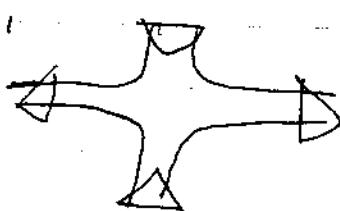


N.B. → why "reconnection"?

N.B. A particular V value is required for stationarity



→ Flow is "stagnation point"



→ How Calculate? → Match In-Flow → Out-Flow
 (S-P. is a great Back-of-Envelope...)

Conserved: ① - mass ($\underline{U} \cdot \underline{V} = 0$)
 ② - momentum in \hat{x} direction (symmetry)
 ③ - energy balance, →
 → rate of field delivery to reconnection region
 MUST BALANCE
 → rate of ohmic dissipation $E_J \sim \underline{A} \underline{J}^2$

$$(1) \quad \begin{array}{ccc} \text{extant in } \hat{x} & & \text{extant in } \hat{y} \\ \{\ & & \{\ \\ \rho_0 V L = \rho_0 V_0 A & & VL = V_0 A \\ \uparrow & & \uparrow \\ \text{inflow} & \text{outflow} & \\ \end{array} \quad \begin{aligned} VL &= V_0 A \\ V &= V_{\text{out}} A / L \end{aligned}$$

$$(2) \quad \rho_0 \left(\frac{\partial \underline{V}}{\partial t} + \underline{V} \cdot \nabla \underline{V} \right) = - \nabla \left(P + \frac{B^2}{8\pi} \right) + \frac{\underline{B} \cdot \nabla \underline{B}}{4\pi}$$

$$\underline{V} \cdot \nabla \underline{V} = - \nabla \left(\frac{V^2}{2} \right) + \underline{V} \times \underline{w}$$

symmetry: $0 = \nabla \left(P + \frac{B^2}{8\pi} + \frac{\rho_0 V^2}{2} \right)$ modified Bernoulli Eq.

$\underbrace{\underline{V}}$ $\rightarrow \underline{V} = 0, B \text{ finite}$
 $\underline{A} = \underline{B}$ $\rightarrow \underline{V} = V_{\text{out}}, B \rightarrow 0$

$$\left(\frac{B^2}{8\pi} \ll P \right)$$

$$\text{So } P + \frac{B^2}{8\pi} + \frac{\rho_0 V^2}{2} = \text{const.}$$

$$P + \frac{B^2}{8\pi} = P + \frac{\rho_0 V_{\text{out}}^2}{2}$$

$$V_{\text{out}}^2 = B^2 / 4\pi\rho_0 = V_A^2$$

\hookrightarrow Al flow speed

$$V_{\text{out}} = V_A$$

$$V = V_A \frac{\Delta}{L}$$

V'' , specifies "speed
in terms Δ .

③



Energy balance

$$\Rightarrow (\text{Rate of Magnetic Energy Inflow}) = (\text{Rate of Ohmic Dissipation, net})$$

$$P_{\text{ohm}} = \frac{J^2}{\tau} \Delta L \text{ so } \dot{E}_{\text{ohm}} = \frac{J^2}{\tau} L \Delta$$

$$= \left(\frac{C}{2\pi}\right)^2 \frac{B^2}{\Delta^2} \frac{L \Delta}{\tau}$$

$$\sigma \times B = \frac{4\pi}{\epsilon} J$$

$$2B = \frac{4\pi J \Delta}{\epsilon}$$

$$P_{\text{in}} = 2 \left(\frac{B^2}{8\pi} \right) VL = \dot{E}_{\text{in}}$$

balance $\Rightarrow 2 \left(\frac{B^2}{8\pi} \right) VL = \frac{C^2}{4\pi} \frac{B^2}{\Delta^2} L \Delta$

$$\frac{C^2}{4\pi\Delta} \equiv \eta \left(\sim \frac{L^2}{\tau} \right)$$

$$V = \left(\frac{C^2}{4\pi\eta} \right) / \Delta \sim \frac{1}{\Delta}$$

$$V = V_A \cdot \Delta / L$$

$$V = M / \Delta$$

$$\Rightarrow \Delta = \left(\frac{M}{V_A} \right)^{1/2} = \left(\frac{L}{R_m} \right)^{1/2}$$

and

$$R_m = \frac{VL}{M} = \text{Magnetic Reynolds \#}$$

(here with $V = V_A$)

$$V = V_A / \sqrt{R_m}$$

\Rightarrow Punch Line : ① - layer is thin $\frac{\Delta}{L} \sim 1/\sqrt{R_m}$

(for large R_m) - speed is faster than $1/L$, } $V \sim V_A / \sqrt{R_m}$
 slower than V_A }

② flow pattern is \approx stagnation \rightarrow { ejection from reconnection layer at V_A

Moral of this story :

\rightarrow freezing-in violated when flows bring opposing \underline{B} into contact




\rightarrow generates singularities \rightarrow thin current layers which alter initial magnetic topology
 \Rightarrow "magnetic reconnection", "tearing", etc.

→ Magnetic Helicity

- another conserved quantity in ideal MHD is magnetic helicity K

$$K = \int_V d^3x \underline{A} \cdot \underline{B}$$

V is taken to be the volume of a 'flux tube'.

- what, yet another invariant?

→ K is different ⇒ has topological interpretation

$$K = \int_V d^3x \underline{A} \cdot \underline{\nabla} \times \underline{A}$$

→ $\underline{x} \rightarrow -\underline{x}$ flips sign of K

→ K is a pseudo-scalar
∴ has orientation or "handedness" --

Proceed via:

- show K conservation
- discuss interpretation of K
- comment on utility ⇒ Taylor Relaxation

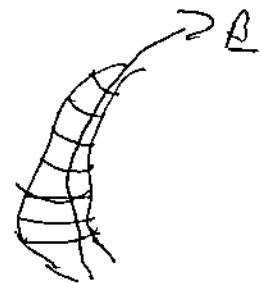
N.B.: Important → K is gauge invariant

i.e. if $\underline{A} \rightarrow \underline{A} + \underline{\nabla} \chi$

$$K \rightarrow K + \int d^3x \underline{\nabla} \underline{A} \cdot \underline{B}$$

$$= K + \int d^3x \underline{\nabla} \cdot (\underline{B} \underline{A})$$

\Rightarrow to surface term. $\left\{ \begin{array}{l} \underline{B} \cdot \hat{n} = 0 \text{ on surface of} \\ \text{tube} \end{array} \right.$



Now, consider a blob of MHD fluid in motion



can show $\frac{dK}{dt} =$

$$\underline{E} + \underline{V} \times \underline{B} = n \underline{J}$$

$$\underline{E} = -\frac{1}{c} \frac{\partial \underline{A}}{\partial t} - \underline{\nabla} \phi$$

\Rightarrow

$$\frac{\partial \underline{A}}{\partial t} = \underline{V} \times \underline{\nabla} \times \underline{A} - c \underline{\nabla} \phi - c n \underline{J}$$

$$\frac{\partial \underline{B}}{\partial t} = -\underline{V} \cdot \underline{\nabla} \underline{B} + \underline{B} \cdot \underline{\nabla} \underline{V} - \underline{B} \underline{\nabla} \cdot \underline{V} + n \underline{\nabla}^2 \underline{B}$$

$$\frac{dK}{dt} = \frac{d}{dt} \int d^3x (\underline{A} \cdot \underline{B})$$

$$= \int d^3x \left(\frac{d\underline{A} \cdot \underline{B}}{dt} + \underline{A} \cdot \frac{d\underline{B}}{dt} \right) + \int \frac{\underline{A} \cdot \underline{B}}{dt} d^3x$$

$$\frac{dK}{dt} = \int d^3x \left(\frac{\partial \underline{A}}{\partial t} \cdot \underline{B} + (\underline{V} \cdot \nabla \underline{A}) \cdot \underline{B} + \underline{A} \cdot \frac{\partial \underline{B}}{\partial t} + \underline{A} \cdot (\underline{V} \cdot \nabla \underline{B}) \right) + \underline{A} \cdot \underline{B} \cdot \nabla \cdot \underline{V}$$

where $\frac{d}{dt} d^3x = \underline{D} \cdot \underline{V}$

i.e. $\frac{d}{dt} d^3x = \frac{d}{dt} d\underline{T} \cdot d\underline{l} + d\underline{T} \cdot \frac{d}{dt} d\underline{l}$
 $= -d\underline{l} \cdot \underline{D} \underline{V} \cdot d\underline{T} + (\underline{D} \cdot \underline{V})(d\underline{T} \cdot d\underline{l}) + d\underline{l} \cdot \underline{D} \underline{V} \cdot d\underline{T}$
 $= \underline{D} \cdot \underline{V} d^3x$ s.t. and $\underline{B} \cdot \underline{n}$ on surface of tube.

$$\frac{dK}{dt} = \int d^3x \left[(\underline{B} \cdot \cancel{\underline{V} \times \underline{B}} - c_f \underline{B} \cdot \nabla \phi - c_M \underline{T} \cdot \underline{B}) + \underline{A} \cdot \underline{V} (\underline{V} \times (\underline{V} \times \underline{B})) + \underline{D} \cdot ((\underline{A} \cdot \underline{B}) \underline{V}) + \underline{A} \cdot \underline{n} \underline{D}^2 \underline{B} \right]$$

where $\underline{A} \cdot (\underline{V} \cdot \nabla \underline{B}) + \underline{B} \cdot (\underline{V} \cdot \nabla \underline{A}) + \underline{A} \cdot \underline{B} \cdot \nabla \cdot \underline{V} = \underline{D} \cdot (\underline{V} \underline{A} \cdot \underline{B})$

$$\frac{dK}{dt} = \int d^3x \left[\underline{D} \cdot ((\underline{A} \cdot \underline{B}) \underline{V}) + \underline{D} \cdot ((\underline{V} \times \underline{B}) \times \underline{A}) + (\underline{V} \times \underline{B}) \cdot (\underline{D} \times \underline{A}) - c_M \underline{T} \cdot \underline{B} - \gamma (\underline{A} \cdot \underline{V} \times \underline{A}) c \right]$$

$$\Rightarrow \frac{d\mathbf{k}}{dt} = \int d^3x \left\{ \underline{\mathbf{D}} \cdot [(\underline{\mathbf{A}} \cdot \underline{\mathbf{B}}) \underline{\mathbf{v}} + (\underline{\mathbf{v}} \times \underline{\mathbf{B}}) \times \underline{\mathbf{A}} + c_1 (\underline{\mathbf{A}} \times \underline{\mathbf{J}})] - c_1 \underline{\mathbf{J}} \cdot \underline{\mathbf{B}} - c_1 \underline{\mathbf{J}} \cdot \underline{\mathbf{B}} \right]$$

$$= \int d\underline{s} \cdot [(\underline{\mathbf{A}} \cdot \underline{\mathbf{B}}) \underline{\mathbf{v}} + (\underline{\mathbf{v}} \times \underline{\mathbf{B}}) \times \underline{\mathbf{A}} + c_1 \underline{\mathbf{A}} \times \underline{\mathbf{J}}] \\ - 2 \int d^3x [c_1 \underline{\mathbf{J}} \cdot \underline{\mathbf{B}}]$$

$$= \int d\underline{s} \cdot [(\cancel{\underline{\mathbf{A}}} \cdot \cancel{\underline{\mathbf{B}}}) \underline{\mathbf{v}} - (\cancel{\underline{\mathbf{A}}} \cdot \cancel{\underline{\mathbf{B}}}) \underline{\mathbf{v}} + (\cancel{\underline{\mathbf{A}}} \cdot \cancel{\underline{\mathbf{B}}}) \underline{\mathbf{B}}] - c_1 \int d\underline{s} \cdot \underline{\mathbf{J}} \times \underline{\mathbf{A}} \\ - 2c_1 \int d^3x (\underline{\mathbf{J}} \cdot \underline{\mathbf{B}}) \quad \cancel{\underline{\mathbf{B}}} \cdot \cancel{\underline{\mathbf{n}}} = 0, \text{ on tube}$$

$$= - \int c_1 d\underline{s} \cdot [\cancel{\underline{\mathbf{B}}} \cdot \underline{\mathbf{A}} - \underline{\mathbf{A}} \cdot \cancel{\underline{\mathbf{B}}}] - 2c_1 \int d^3x \underline{\mathbf{J}} \cdot \underline{\mathbf{B}}$$

$$= - 2c_1 \int d^3x (\underline{\mathbf{J}} \cdot \underline{\mathbf{B}})$$

\Rightarrow have shown:

$$\boxed{\frac{d\mathbf{k}}{dt} = - 2c_1 \int d^3x (\underline{\mathbf{J}} \cdot \underline{\mathbf{B}})}$$

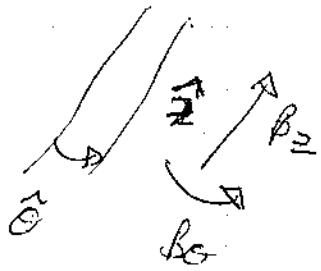
and clearly! $\frac{d\mathcal{H}}{dt} \rightarrow 0$ as $J \rightarrow 0$
 (non-singular J)

Magnetic Helicity is conserved in ideal MHD.

→ Magnetic Helicity conserved, but what does it mean?

- helicity is non-trivial \Rightarrow more than just helical field lines.

interesting to note: $\mathcal{H}(r) = \frac{rB_z}{RB_\theta(r)} = \frac{1}{R\mu(r)}$



$$\mu(r) = \frac{B_\theta(r)}{rB_z} \rightarrow \text{field line pitch.}$$

cylindrical plasma $\rightarrow B = B(r)$

(length scale at which winding varies)

$$\text{Now, } A_\theta = \frac{1}{r} \int_0^r B_z dr$$

$$A_z = - \int_0^r B_\theta dr$$

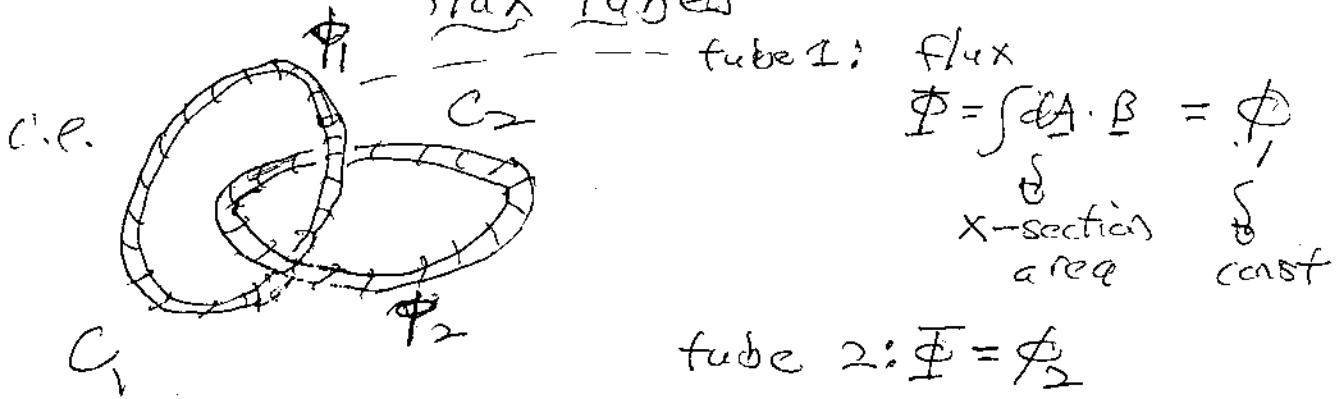
$$\underline{\underline{so}} \quad \underline{\underline{A}} \cdot \underline{\underline{B}} = \frac{B_0}{r} \int_0^r B_z dr - B_z \int_0^r \frac{B_0}{r} dr \\ = \mu B_z \int_0^r \frac{B_0}{\mu} dr - B_z \int_0^r \frac{B_0}{r} dr$$

$$\underline{\underline{A}} \cdot \underline{\underline{B}} = B_z \left[\mu \int_0^r \frac{B_0}{\mu} dr - \int_0^r \frac{B_0}{r} dr \right]$$

$= 0$ for constant μ

\therefore non-zero helicity requires $\mu = \mu(r)$
 i.e. — pitch varies with radius
 \Rightarrow magnetic shear

- physically \rightarrow helicity means self-linkage of 2 flux tubes



field in loops, only

Now, for volume V_1 of tube I

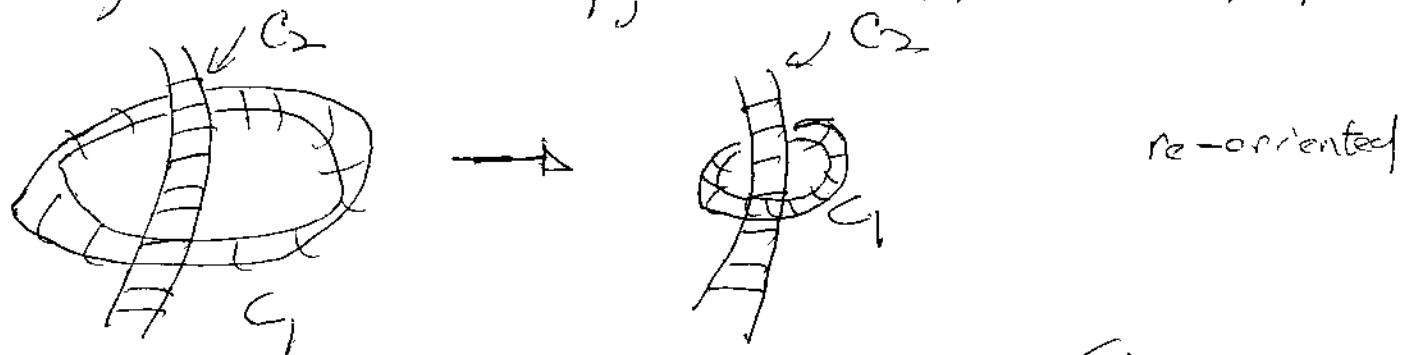
$$k = \int_{V_1} A \cdot B \, d^3x = \oint dl \int_{\text{ols}} A \cdot B$$

C_1
 ↓
 along
 100A
 {
 X-set
 area

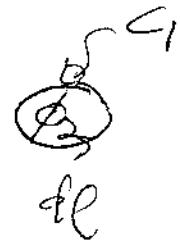
$$= \oint_{C_1} A \cdot dl \int_{S_1} B \cdot \hat{n} \, dA$$

$$= \oint_{C_1} \oint_{C_2} A \cdot dl$$

Now, can shrink C_1 , as no field outside loops



→ in x section:



$$\text{but } \oint_{C_1} A \cdot dl = \int_{A \text{ enclosed}} B \cdot dS = \oint_{C_2}$$

$$so \dots k_1 = \phi_1 \phi_2 \rightarrow \text{product of fluxes}$$

similarly

$$k_2 = \phi_2 \phi_1$$

$$\therefore k = 2\phi_1 \phi_2$$

$$\text{if } n \text{ windings} \quad k = k_1 + k_2 = \pm 2n\phi_1 \phi_2$$

\Rightarrow helicity is measure of self-linkage of magnetic configuration.

Why care \rightarrow Taylor Conjecture (1974)
(J.B. Taylor)

- in magnetic confinement, of great interest to determine how fields, currents self-organize

- RFP



\sim toroid

\sim toroidal current

$$\text{well fit by } B_z = B_0 J_0 (\propto r) \quad \underline{J} \times \underline{B} = 0$$

$$B_\theta = B_0 J_1 (\propto r)$$



force free

\Rightarrow why so robust
especially since RFP's are turbulent

- Taylor conjectured conservation of magnetic helicity constraints relaxation to force-free state.

Key Point - helicity conserved in flux tubes to if

- toroidal plasma \rightarrow many small tubes



etc.

- recall Sweet-Parker model:
magnetic reconnection / resistive dissipation effective on small scales.

\Rightarrow Taylor Conjecture: At finite N , helicity of small tubes dissipated but) global, helicity conserved.

$$\text{c.e.} \quad \int \underline{\mathbf{A}} \cdot \underline{\mathbf{B}} \, d^3x = h_0 \rightarrow \textcircled{a} \text{ conserved.}$$

\checkmark

plasma volume

\therefore Taylor conjectured that optical magnetic configuration could be explained by minimum principle:

$$\delta \left[\int d^3x \frac{B^2}{8\pi} + \lambda \int d^3x \underline{A} \cdot \underline{B} \right] = 0$$

i.e. minimize magnetic energy subject to constraint of conserved global helicity.

Comments:

- it works! - indeed amazingly well - for RFPs, spheromaks, etc. Departures only recently being discovered
- inspired idea of helicity injection as way to maintain configurations
- it is a conjecture → no proof.
 Hypothesis: Selective Decay
 - energy cascades
 - small scale
 - helicity cascades
 - large scale (less dissipation)
- relevance to driven system?
 i.e. in real RFP, transformer on.

- dynamics? - how does relaxation occur
→ more in discussion of kinks,
tearing..